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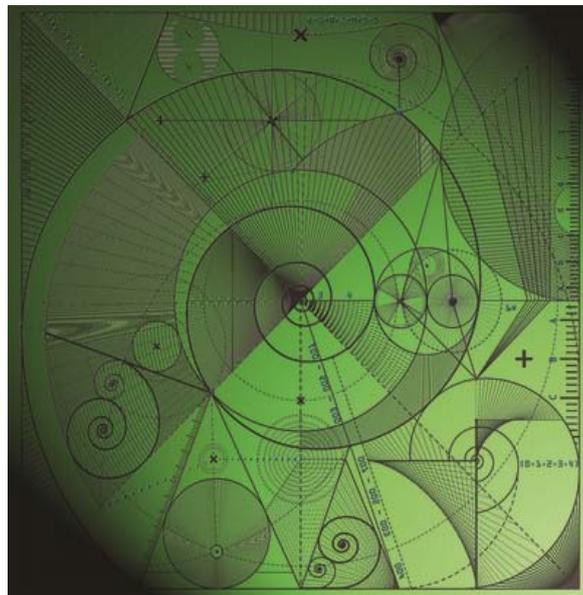
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Surface permeability, capillary transport and the Laplace-Beltrami problem

by

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We have established previously, in a lead-in study, that the spreading of liquids in particulate porous media at low saturation levels, characteristically less than 10% of the void space, has very distinctive features in comparison to that at higher saturation levels. In particular, we have found that the dispersion process can be accurately described by a special class of partial differential equations, the super-fast non-linear diffusion equation. The results of mathematical modelling have demonstrated very good agreement with experimental observations. However, any enhancement of the accuracy and predictive power of the model, keeping in mind practical applications, requires the knowledge of the effective surface permeability of the constituent particles, which defines the global, macroscopic permeability of the particulate media. In the paper, we demonstrate how this quantity can be determined through the solution of the Laplace-Beltrami Dirichlet problem, we study this using the well-developed surface finite element method.

I. INTRODUCTION

Liquid distributions and transport in particulate porous media, such as sand, at low saturation levels s , defined in our study as the ratio of the liquid volume V_L to the volume of available voids V_E in a sample volume element V , $s = \frac{V_L}{V_E}$, have many distinctive features. Theoretically, as we have shown previously, the liquid dispersion can be described by a special class of mathematical models, the superfast non-linear diffusion equation [1]. Unlike in the standard porous medium equation, which is a paradigm of research in porous media [2], in this special case, the non-linear coefficient of diffusion $D(s)$ demonstrates divergent behaviour as a function of saturation s , $D(s) \propto (s - s_0)^{-3/2}$, where s_0 is some minimal saturation level.

In practical applications, the analysis of this regime of wetting is crucial for studies of biological processes, such as microbial activity, and spreading of persistent (non-volatile) liquids in soil compositions and dry porous media commonly found in arid natural environments and industrial installations [1, 3].

If we consider liquid distributions on the grain size length scale, one would observe that when the saturation level s is reduced to (or below) the critical level $s_c \approx 10\%$, the liquid domain predominantly consists of isolated liquid bridges formed at the point of particle contacts [1, 4–8], see Fig. 1 for illustration. The formation of liquid bridges is characteristic for the so-called pendular regime of wetting. In this regime, the liquid bridges are only connected via thin films formed on the rough particle surfaces and serve as variable volume reservoirs, where the capillary pressure p depends directly on the amount of the liquid in the bridge V_b

$$p \approx -p_0 \left(\frac{R^3}{V_b} \right)^{1/2}. \quad (1)$$

Here, $p_0 = \frac{2\gamma}{R}$, γ is the coefficient of the surface tension of the liquid and R is an average radius of the porous medium particles [1, 4]. The spreading process in such

conditions only occurs over the rough surface of the elements of the particulate porous media, Fig. 1.

Microscopically, the liquid creeping flow through the surface roughness of each particle can be described by a local Darcy-like relationship between the surface flux density \mathbf{q} and averaged (over some area containing many surface irregularities) pressure in the grooves ψ

$$-\frac{\kappa_m}{\mu} \nabla \psi = \mathbf{q}. \quad (2)$$

Here, μ is liquid viscosity and κ_m is the local coefficient of permeability of the rough surface, which proportional to the average amplitude of the surface roughness δ_R , that is the width of the surface layer conducting the liquid flux, $\kappa_m \propto \delta_R^2$ [9].

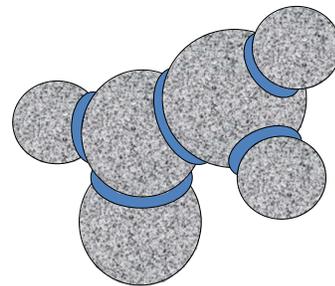


FIG. 1. Illustration of the liquid distribution in particulate porous media (grey) with pendular rings (blue) at low saturation levels.

Macroscopically, that is after averaging over some volume element containing many particles of the porous medium, the diffusion process in the slow creeping flow conditions can be described by a non-linear superfast diffusion equation

$$\frac{\partial s}{\partial t} = \nabla \{D(s) \nabla s\}, \quad t > 0, \quad (3)$$

$$D(s) = \frac{D_0}{(s - s_0)^{3/2}}, \quad s > s_0,$$

which directly follows from the conservation of mass principle

$$\frac{\partial(\phi s)}{\partial t} + \nabla \mathbf{Q} = 0. \quad (4)$$

Here D_0 is the effective, macroscopic coefficient of non-linear diffusion, s_0 is the minimal level of saturation, which can be only achieved when the liquid bridges cease to exist ($s_0 \approx 0.5\%$, see details in [1, 7, 8]), ϕ is porosity defined as $\phi = \frac{V_E}{V}$, which is further assumed to be constant, and \mathbf{Q} is macroscopic flux density. The macroscopic flux density \mathbf{Q} is defined in such a way that the total flux through the surface of a macroscopic sample volume element is given by the surface integral $\int \mathbf{Q} \cdot \mathbf{n} dS$, where \mathbf{n} is the normal vector to the surface of the element.

Equation (3) can be obtained from (4) using (1)-(2) and the spatial averaging theorem formulated in [13] assuming that [1]:

- the rough surface area of the porous media particles is fully saturated with the liquid;
- the liquid is incompressible;
- the local Darcy's law (2) is observed on the rough particle surface elements.

All three criteria are usually very well satisfied in practical applications, and we will further assume that this is the case. The approximation of the fully saturated rough surface layer is well fulfilled, if the characteristic pressure ψ is less than the capillary pressure defined on the length scale of the surface roughness δ_R , which is of the order of $\delta_R \sim 1 \mu\text{m}$ in typical sands [14], as is demonstrated in [9]. That is, $|\psi| < \frac{\gamma}{\delta_R}$, and, for example for water ($\gamma = 72 \text{ mN/m}$) at $\delta_R = 1 \mu\text{m}$, this results in $|\psi| < 7.2 \times 10^4 \text{ Pa}$. Otherwise, at larger capillary pressure values, the liquid volume within the surface roughness layer would start to vary leading to variations of the effective surface layer thickness δ_R , though, it is not difficult to introduce a correction [3, 10–12].

The effective coefficient of diffusion $D_0 = f_\phi \frac{K}{\mu}$ comprises of the global permeability of the surface elements $K = k_m \frac{S_e}{S}$ [1]. Here, parameter $f_\phi = \frac{p_0}{2\phi} \sqrt{\frac{3N_c}{4\pi} \frac{1-\phi}{\phi}}$, N_c is a coordination number of the particles, that is average number of contacts per a particle (in sands, typically, $N_c \approx 7$) and S_e/S is the ratio of the effective area of entrances and exits of the liquid flow in a sample volume element with surface area S , see details in [1]. Note, that the ratio S_e/S is defined in such a way, that the microscopic flux density \mathbf{q} averaged over the liquid volume V_i within a macroscopic sample volume element V , $\langle \mathbf{q} \rangle^l = \int_{V_i} \mathbf{q} dV$, if multiplied by the ratio $\langle \mathbf{q} \rangle^l \frac{S_e}{S} = \mathbf{Q}$, would result in the macroscopic average flux density \mathbf{Q} .

The global surface permeability of the particles K is one of the main elements of the model that enables an accurate representation of the liquid dispersion at low saturation levels. On the other hand, this quantity is difficult to accurately estimate a priori. It is fully defined by the particle shape and the dimension of the liquid bridge area. In this paper, we determine this important parameter on the basis of a solution to the Laplace-Beltrami problem in a representative case of a spherical particle, which provides a reasonable approximation for the constituent elements of particulate porous media, such as sands.

II. MICROSCOPIC MODEL OF THE SURFACE PERMEABILITY OF THE ELEMENTS.

Consider a spherical particle of radius R with a closed surface Γ , which is split into three sub-domains Ω_0 , Ω_1 and Ω_2 with the surface boundaries between them $\partial\Omega_1$ and $\partial\Omega_2$, as is shown in Fig. 2. The location of the sub-domains Ω_1 and Ω_2 to each other on the surface is fixed by the tilt angle α . The sub-domains Ω_1 and Ω_2 correspond to the area covered by the liquid in the bridges, while the surface flow, described by (2), takes place in Ω_0 .

Since the rough surface area of the particles is assumed to be fully saturated in creeping flow conditions [9], liquid pressure ψ , due to incompressibility of the liquid, should satisfy the Laplace-Beltrami equation defined on the surface of the sub-domain Ω_0

$$\Delta_{\Omega_0} \psi = 0, \quad (5)$$

as it follows from (2). Here, Δ_{Ω_0} designates the Laplace-Beltrami operator, which is defined on the surface element Ω_0 through the surface gradient ∇_{Ω_0} tangential to the surface. Formally, let \mathbf{n}_{Ω_0} denote the unit normal to the surface Ω_0 then we define the surface gradient of ψ as $\nabla_{\Omega_0} \psi := \nabla \psi - (\nabla \psi \cdot \mathbf{n}_{\Omega_0}) \mathbf{n}_{\Omega_0}$ and then the Laplace-Beltrami operator is defined as $\Delta_{\Omega_0} \psi = \nabla_{\Omega_0} \cdot \nabla_{\Omega_0} \psi$.

Note, that in fact, the condition of the fully saturated surface layer is not essential in calculation of the flows over one particle element of the porous media. It is sufficient to presume that the variation of the capillary pressure on the length scale of the particle $\delta\psi$ is negligible, that is $\delta\psi \ll \gamma/\delta_R$. This is usually the case in slow creeping flow conditions in porous media, and in fact, it is a criterion for the use of macroscopic approximation to such flows [15].

At the same time, liquid pressure variation in the bridges is negligible in slow creeping flows in comparison to that in Ω_0 . So that, one can assume that

$$\psi|_{\partial\Omega_1} = \psi_1 = \text{const}, \quad \psi|_{\partial\Omega_2} = \psi_2 = \text{const}, \quad (6)$$

which are the boundary conditions to the Laplace-Beltrami Dirichlet boundary value problem. The Dirichlet boundary value problem (5)-(6) has a unique solution,

which, if it is found, allows to calculate the total flux through the particle element

$$Q_T = \delta_R \frac{\kappa_m}{\mu} \int_{\partial\Omega_1} \frac{\partial\psi}{\partial n} dl = -\delta_R \frac{\kappa_m}{\mu} \int_{\partial\Omega_2} \frac{\partial\psi}{\partial n} dl,$$

where \mathbf{n} is the normal vector to the domain boundaries $\partial\Omega_{1,2}$ on the surface, δ_R is the average amplitude of the surface roughness, that is the width of the surface layer conducting the liquid flux and the line integral is taken along a closed curve in Ω_0 , for example the boundary $\partial\Omega_1$.

If the total flux Q_T is determined, one can define the global permeability coefficient of a single particle K_1 . This can be done, if we assume that the particle has a characteristic size D and so that it can be enclosed in a volume element $V = D^3$ with the characteristic side surface area D^2 . Then, the effective flux density Q can be represented in terms of K_1 (and the total flux Q_T)

$$Q = \frac{Q_T}{D^2} = -\frac{K_1}{\mu} \frac{\psi_2 - \psi_1}{D},$$

if the flow is driven by the constant pressure difference $\psi_2 - \psi_1$ applied to the sides of the volume element.

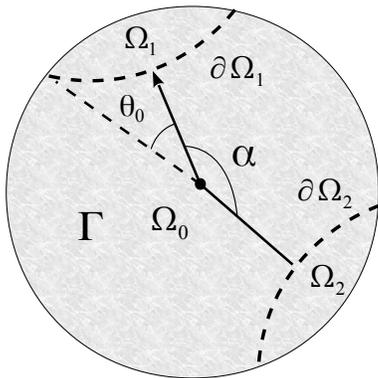


FIG. 2. Illustration of the solution domains on a spherical particle.

A. Surface permeability of a sphere in the case of azimuthally symmetric domain boundaries.

Consider now an azimuthally symmetric case, when the domain boundaries $\partial\Omega_1$ and $\partial\Omega_2$ are oriented at the reflex angle $\alpha = \pi$ and have a circular shape. We use a spherical coordinate system with its origin at the particle centre and the polar angle θ counted from the axis of symmetry passing through the centre of the circular contour $\partial\Omega_1$. In this case, the Dirichlet boundary value problem (5)-(6) admits an analytical solution, so that particle permeability can be determined explicitly. Indeed, problem

(5)-(6), if we assume that the liquid pressure ψ is a function of θ only and independent of the azimuthal angle, is equivalent to

$$\frac{1}{\sin\theta} \frac{\partial}{\partial\theta} \left(\sin\theta \frac{\partial\psi}{\partial\theta} \right) = 0, \quad \theta_0 < \theta < \pi - \theta_1, \quad (7)$$

with the boundary conditions

$$\psi|_{\theta=\theta_0} = \psi_1, \quad \psi|_{\theta=\pi-\theta_1} = \psi_2. \quad (8)$$

The analytic solution to problem (7)-(8) after applying the boundary conditions can be represented in the following form

$$\psi = \Psi_0(\psi_2 - \psi_1) \ln \left\{ \frac{\sin\theta}{\sin\theta_0} \frac{1 + \cos\theta_0}{1 + \cos\theta} \right\} + \psi_1, \quad (9)$$

where

$$\Psi_0 = \frac{1}{\ln \left\{ \frac{\sin\theta_1}{\sin\theta_0} \frac{1 + \cos\theta_0}{1 - \cos\theta_1} \right\}}.$$

One can now calculate the total flux

$$\begin{aligned} Q_T &= -\frac{K_1}{\mu} D(\psi_2 - \psi_1) = -2\pi \sin\theta_0 \delta_R \frac{k_m}{\mu} \frac{\partial\psi}{\partial\theta} \Big|_{\theta=\theta_0} \\ &= -(\psi_2 - \psi_1) 2\pi \delta_R \Psi_0 \frac{k_m}{\mu}. \end{aligned}$$

So that, taking $D = 2R$,

$$K_1 = \pi \Psi_0 \frac{\delta_R}{R} k_m. \quad (10)$$

One can see that, if we take $\theta_1 = \theta_0$, the permeability coefficient K_1 is divergent at $\theta_0 = \pi/2$, as is expected, when the two contours move closer to each other and, at the same time, their radius $R \sin\theta_0$ increases, that is

$$K_1 \approx \frac{\delta_R}{2R} \frac{\pi k_m}{\left(\frac{\pi}{2} - \theta_0\right)} \text{ as } \theta_0 \rightarrow \frac{\pi}{2}.$$

In the opposite limit, at $\theta_0 = 0$, when the two contours move further away from each other and their radius decreases, the permeability coefficient tends to zero, that is

$$K_1 \approx \frac{\delta_R}{2R} \frac{\pi k_m}{|\ln\theta_0|} \text{ as } \theta_0 \rightarrow 0.$$

Parametrically, the coefficient of permeability (10) is inversely proportional to the particle radius R , so that larger particles create stronger resistance to the flow. Noticeably, the coefficient demonstrates strong dependence on the surface layer thickness δ_R , that is $K_1 \propto \delta_R^3$ since it is anticipated that $k_m \propto \delta_R^2$, so that evaluation of this parameter in applications is crucial for the accurate estimates of the liquid dispersion rates.

How does the result affect the super-fast diffusion model (3), and basically how can it be incorporated into the main diffusion equation? If we approximate the permeability coefficient K by K_1 obtained in the azimuthally symmetric case at $\theta_1 = \theta_0$, and, using an approximate relationship between the radius of curvature $R \sin \theta_0$ of the boundary contour $\partial\Omega_1$ and the pendular ring volume [6], one can show

$$\sin^2 \theta_0 \approx \sqrt{s - s_0}$$

and at $\theta_0 \ll 1$ or $(s - s_0) \ll 1$

$$K \approx 2 \frac{\delta_R}{R} \frac{\pi k_m}{|\ln(s - s_0)|}. \quad (11)$$

As one can see from (11), the distinctive particle shape results in logarithmic correction to the main non-linear superfast-diffusion coefficient $D(s) = \frac{D_0}{(s - s_0)^{3/2}}$, such that

$$D(s) \propto \frac{1}{|\ln(s - s_0)|(s - s_0)^{3/2}}.$$

Apparently, the correction will mitigate to some extent the divergent nature of the dispersion at the very small saturation levels $s \approx s_0$, smoothing out the characteristic dispersion curves.

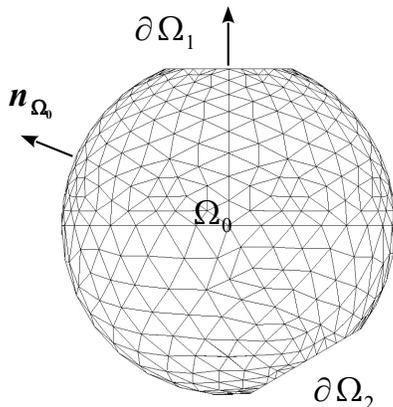


FIG. 3. Illustration of the triangular tessellation of the truncated spherical surface domain Ω_0 with a normal vector \mathbf{n}_{Ω_0} at $\alpha = 150^\circ$ and $\theta_0 = \theta_1 = 22.5^\circ$.

Before we proceed to a general case, this would be instructive to consider, in qualitative terms, how specific is the permeability of spherical particles. We now compare coefficient of permeability (10) with the permeability of a cylinder of radius $R \sin \theta_0$ and length $2R$ with the same surface layer of thickness δ_R . Such an element was often used in simple estimations of permeability in porous media [16]. It is not difficult to calculate the total flux

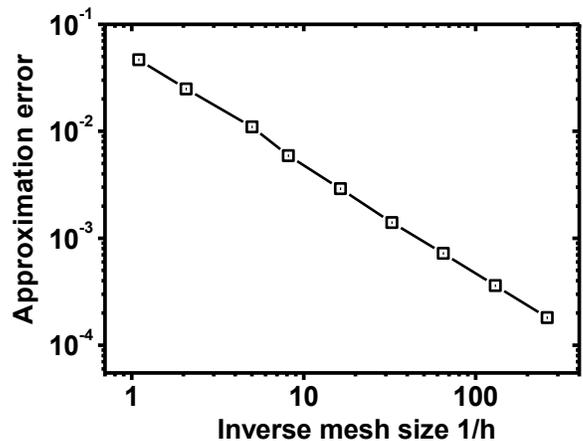


FIG. 4. Verification of the numerical scheme in the azimuthally symmetric scenario. We plot the inverse mesh size against the error measured in the energy norm [17]. We observe the rate of convergence proven in [17] verifying that, asymptotically, the numerical approximation converges to the exact solution.

through this element when there is a constant pressure difference $(\psi_2 - \psi_1)$ applied to its ends

$$Q_T = -(\psi_2 - \psi_1) \frac{k_m}{\mu} \pi \sin \theta_0 \delta_R = -\frac{K_c}{\mu} 2R(\psi_2 - \psi_1),$$

so that

$$K_c = \pi k_m \sin \theta_0 \frac{\delta_R}{2R} \propto (s - s_0)^{1/4},$$

where K_c is the effective permeability of the cylindrical element.

One can observe, that in contrast to the case of spherical elements, the cylindrical approximation provides completely different correction to the non-linear coefficient of diffusion, if we presume similar scaling $\sin^2 \theta_0 \approx \sqrt{s - s_0}$. Consider now a general case.

B. Surface permeability of a sphere in the case of arbitrary oriented boundaries.

In the arbitrary case, when $\alpha \neq \pi$, the Dirichlet boundary value problem (5)-(6) does not possess known explicit solutions, so that we will apply a classical surface finite element technique introduced in [17]. See also [18] for an in depth review of state of the art innovations and uses pertaining to this class of method. Using this method we are able to numerically investigate the total flux and hence the permeability of the particle.

We begin by approximating the truncated spherical surface with a piecewise linear approximation through triangular elements, see Fig. 3 for an example. In this setting, we are approximating the geometry with a polygon. This inherently introduces an error through the

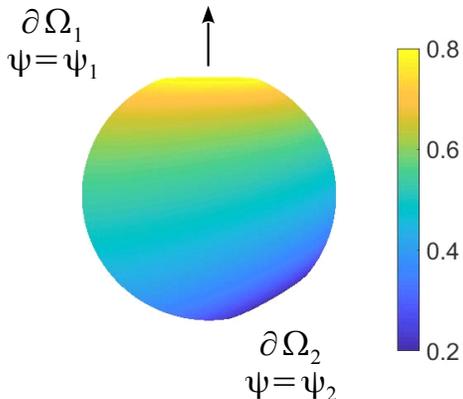


FIG. 5. Distribution of non-dimensional pressure ψ/ψ_c ($\psi_c = \gamma/R$) on a unit sphere $R = 1$ at $\psi_1 = 0.8$, $\psi_2 = 0.2$, $\theta_1 = \theta_0 = 22.5^\circ$ and $\alpha = 150^\circ$.

approximation of the geometry. It is, however, well understood appearing as a 'variational crime' [18]. We then discretise the Laplace-Beltrami operator over the polygon using piecewise linear finite elements. To test our numerical model we examine the azimuthally symmetric case, where the exact solution is known and given in (9). We then check convergence of the finite element approximation to (9). The results are shown in Fig. 4.

We make use of the numerical model generated to examine the dependency of the total flux, and hence the permeability of the truncated spherical element as a function of the tilt angle α , that is the position of the boundaries on the sphere. As in the azimuthally symmetric case, without much loss of generality, we consider circular boundaries. The size of the boundary contour, that is its radius $R \sin \theta_0$ (or $R \sin \theta_1$), will be characterized by the polar angle θ_0 (or θ_1) counted from the axis of symmetry of each contour and the particle radius R .

C. Results of numerical analysis and discussion

The distribution of pressure on the spherical surface is illustrated in Fig. 5, while the typical total flux dependence on the tilt angle α is presented in Fig. 6 at $\theta_0 = \theta_1$. The distribution of pressure demonstrates relatively smooth variations in the range bounded by the prescribed boundary values, such that, as is expected in a diffusion problem, $\psi_2 \leq \psi \leq \psi_1$. The value of the total liquid flux Q_T through the spherical element decreases when the tilt angle increases and the boundary contours move further away from each other. At the same time, one readily observes, Fig. 6, that at relatively large tilt angles, close to the reflex angle in the azimuthal symmet-

rical case, the total flux value and hence permeability of the surface elements, is close to that predicted on the basis of the azimuthally symmetric solution (10). This implies that the analytical result (10) and (11) can be used in practical applications to obtain first order corrections to the effective non-linear coefficient of dispersion in the super-fast diffusion model. One may notice that even at small tilt angles, when the two boundaries are located close to each other, one can still approximate coefficient of permeability with the accuracy of 50%. We have verified numerically that in the general case the permeability coefficient of the particles demonstrates the same trends with variations of parameters θ_0 and θ_1 as in the azimuthally symmetric case.

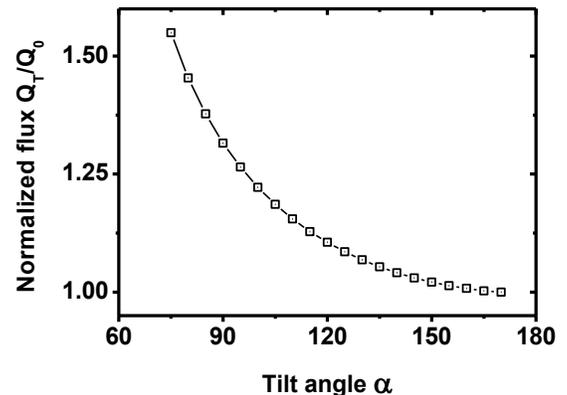


FIG. 6. Non-dimensional total flux Q_T/Q_0 as a function of the tilt angle α at $\theta_0 = \theta_1$. Here Q_0 is the total flux value at $\alpha = 180^\circ$.

CONCLUSIONS

We have demonstrated how the permeability coefficient of constituent particle surface elements of a porous matrix can be estimated on the basis of a solution to the Laplace-Beltrami problem using, as an example, truncated spherical particles with arbitrary oriented boundaries. In the azimuthally symmetric case, we obtained an observable analytical solution, which has been incorporated into the macroscopic super-fast dispersion model to calculate a correction to the effective non-linear coefficient of diffusion. We have shown, that in the case of arbitrary oriented boundaries, the analytical solutions provide a reasonable approximation in the general case. The analytical, (10) and (11), and numerical solutions are the main results of our paper. The methodology developed in our study can be used in practical applications involving more sophisticated shapes of constituent elements. This will be the subject of future studies.

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